Zagazig University, Faculty of Engineering Final Exam Academic Year: 2016/2017 Specialization: Computer & Systems Eng. Course Name: Robotics Course Name: CSE629/CSE514/CSE513 Examiner: Dr. Mohammed Nour



Date: 04/02/2017 Exam Time: 3 hours No. of Pages: 9 No. of Questions: 5 Full Mark: [70]

 \triangleright Please **answer all questions**. Use **3** decimal digits approximation. ▷ Use your answer sheet as a draft for solutions. Attach last exam page to it. \triangleright Mark your answers for all questions in the table provided in the last page. Question 1. [16 Marks] (2×8) 1. Which of the following terms refers to the rotational motion of a robot arm? a) swivel b) axle c) roll d) vaw 2. What is the name for the space inside which a robot unit operates? b) spatial base d) work envelop a) environment c) danger zone 3. Which of the following terms is not one of the five basic parts of a robot? a) peripheral tools b) end effectors c) controller d) sensor 4. The number of moveable joints in the base, the arm, and the end effectors of the robot determines? a) degrees of freedom b) operational limits c) flexibility d) cost 5. For a robot unit to be considered a functional industrial robot, typically, how many degrees of freedom would the robot have? a) three b) four c) six d) eight 6. Which of the basic parts of a robot unit would include the computer circuitry that could be programmed to determine what the robot would do? c) end effector d) drive a) controller b) arm 7. End effectors can be classified into two categories which are... a) elbows and wrists b) grippers and end of arm tooling c) grippers and wrists d) end of arm tooling and elbows 8. The amount of weight that a robot can lift is called... b) payload c) dead lift d) horsepower a) tonnage Question 2. [8 Marks] (2×4) Υ A 2-DOF planar manipulator has a rotational joint and a prismatic

joint. The two links are perpendicular to each other and their dimensions are as indicated. P is the tip (end-effector) of the manipulator.



9. This manipulator workspace is sketched as:



10. The dimensions of the workspace can be mathematically expressed as:

a)
$$x^2 + y^2 \le 8a^2$$

b) $x + y \le a\cos\theta$
c) $a^2 \le x^2 + y^2 \le (3a)^2$
d) $x \le 2\sqrt{2}a$ and $y \le a$

Solution

The Cartesian workspace sketch is shown in the figure in shadowed area.



Question 3. [10 Marks]

(2+2+1+1+2+2)

Consider the pose of the objects A and B in space, as shown on the left. The goal is to displace object B into a new pose \mathbf{C} on A, so that both objects are connected as shown on the right:



11. The homogeneous transformation matrix \mathbf{H}_B^0 to represent **B** w.r.t. frame 0 is:

$$a) \begin{bmatrix} 1 & 0 & 0 & 3 \\ 0 & \frac{1}{\sqrt{2}} & -\frac{1}{\sqrt{2}} & 2 \\ 0 & \frac{1}{\sqrt{2}} & \frac{1}{\sqrt{2}} & 1 \\ 0 & 0 & 0 & 1 \end{bmatrix} b) \begin{bmatrix} -1 & 0 & 0 & 0 \\ 0 & -1 & 0 & 5 \\ 0 & 0 & 1 & -1 \\ 0 & 0 & 0 & 1 \end{bmatrix} c) \begin{bmatrix} 1 & 0 & 0 & 3 \\ 0 & -1 & 0 & 2 \\ 0 & 0 & -1 & 1 \\ 0 & 0 & 0 & 1 \end{bmatrix} d) \begin{bmatrix} 1 & 0 & 0 & -3 \\ 0 & -1 & 0 & 8 \\ 0 & 0 & -1 & 3 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

12. The homogeneous transformation matrix \mathbf{H}_{C}^{0} to represent C w.r.t. frame 0 is:

$$\mathbf{a} \right) \begin{bmatrix} 1 & 0 & 0 & 3 \\ 0 & \frac{1}{\sqrt{2}} & -\frac{1}{\sqrt{2}} & 2 \\ 0 & \frac{1}{\sqrt{2}} & \frac{1}{\sqrt{2}} & 1 \\ 0 & 0 & 0 & 1 \end{bmatrix} \mathbf{b} \right) \begin{bmatrix} -1 & 0 & 0 & 0 \\ 0 & -1 & 0 & 5 \\ 0 & 0 & 1 & -1 \\ 0 & 0 & 0 & 1 \end{bmatrix} \mathbf{c} \right) \begin{bmatrix} 1 & 0 & 0 & 3 \\ 0 & -1 & 0 & 2 \\ 0 & 0 & -1 & 1 \\ 0 & 0 & 0 & 1 \end{bmatrix} \mathbf{d} \right) \begin{bmatrix} 1 & 0 & 0 & -3 \\ 0 & -1 & 0 & 8 \\ 0 & 0 & -1 & 3 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

13. A sequence of transformations that reaches the desired pose is:

a)
$$\mathbf{C} = T(3, 2, 1) R_x \left(\frac{\pi}{2}\right)$$

b) $\mathbf{C} = T(-3, 0, -1) R_x \left(\frac{\pi}{2}\right)$
c) $\mathbf{C} = T(3, 2, 1) R_x(\pi)$
d) $\mathbf{C} = T(0, -5, 1) R_x(\pi)$

Consider the following homogeneous transformation matrix \mathbf{F} and rotation matrix \mathbf{R} :

$\mathbf{F} =$	$\begin{bmatrix} x_1 \\ x_2 \\ x_3 \\ 0 \end{bmatrix}$	$ \begin{array}{c} 0 \\ 0 \\ -1 \\ 0 \end{array} $	$-1 \\ 0 \\ 0 \\ 0 \\ 0$	5 3 2 1	$\mathbf{R} = \begin{bmatrix} x_1 & 0 & - \\ x_2 & 0 & 0 \\ x_3 & -1 & 0 \end{bmatrix}$	-1))
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14. We can split the transformation matrix \mathbf{F} into:

a) $\begin{bmatrix} 0 & -1 & 5 \\ 0 & 0 & 3 \\ -1 & 0 & 2 \end{bmatrix}$ and $\begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix}$

c) translation followed by a rotation

15. In the rotation matrix \mathbf{R} :

a)
$$Rank(\mathbf{R}) = 4$$

- b) $\mathbf{R}\mathbf{R}^T = \mathbf{I}$ c) dot product of any two columns is one
 - d) cross product of any two rows is zero

b) $\begin{bmatrix} x_1 & 0 & -1 \\ x_2 & 0 & 0 \\ x_3 & -1 & 0 \end{bmatrix}$ and $\begin{bmatrix} 5 \\ 3 \\ 2 \end{bmatrix}$

d) both b) and c)

16. In the rotation matrix **R**, values of x_1, x_2 and x_3 are calculated as:

a) 1,0,0 b)	0, 1, 0	c) $0, 0, 1$	d) 1, 1, 1
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Solution

We can select an arbitrary sequence of displacements, where object B is first rotated for 180° about axis x_0 . It is easy to realize, that we shall reach the final pose C using translations only.

The object is first lifted for at least 1 unit in z_0 direction, in order not to collide with object A. Afterwards we slide over object A for 3 units in the x_0 direction. After displacing the object for two units in y_0 direction, the objects A and B are connected. As we are dealing with a transformations in a reference frame, the individual transformations are written in reverse order:

$$\mathbf{C} = T(3,2,1) R_x(\pi)$$

Since \mathbf{R} is a rotation matrix, then:

$$\mathbf{RR}^{T} = \mathbf{I}$$

$$\begin{bmatrix} x_{1} & 0 & -1 \\ x_{2} & 0 & 0 \\ x_{3} & -1 & 0 \end{bmatrix} \begin{bmatrix} x_{1} & x_{2} & x_{3} \\ 0 & 0 & -1 \\ -1 & 0 & 0 \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

from which we get:

$$\begin{aligned} x_1^2 + 1 &= 1 \quad \Rightarrow \quad x_1 = 0 \\ x_2^2 &= 1 \quad \Rightarrow \quad x_2 = 1 \\ x_3^2 + 1 &= 1 \quad \Rightarrow \quad x_3 = 0 \end{aligned}$$

Note that $x_2 = -1$ is rejected because for a rotation matrix |R| = 1 as $\mathbf{R} \in SO(3)$ With the above solution can very that:

$$x_1 x_2 = 0, \quad x_1 x_3 = 0, \quad x_3 x_2 = 0$$

Question 4. [12 Marks

(2+2+4+4)

Consider the slider-crank mechanism shown below with θ_1 as **actuated** joint and $\{x_S, y_S\}$ is the base frame and $\{x_T, y_T\}$ is the tool frame:



17. This mechanism has degrees of freedom.

a) one b) two c) three d) four

- 18. Gruebler formula **can not** be used because:
 - a) the mechanism moves in one dimension (in the x-axis direction) only.
 - b) it is used with 2D parallel mechanisms.
 - c) it is used with either 3D closed chains manipulators.
 - d) it is applicable for inverse kinematics.
- 19. the manipulator forward kinematics (i.e. given θ_1 find $\begin{bmatrix} x_T & y_T \end{bmatrix}^T$)

a)
$$a_3 + \frac{a_2 \sin(\theta_1 + \theta_2)}{\sin \theta_1}$$
 b) $\frac{a_2 \sin(\theta_1 + \theta_2)}{\sin \theta_1}$ c) $a_2 \sin(\theta_1 + \theta_2)$ d) $d \sin(\theta_1)$

- 20. the manipulator inverse kinematics (i.e. given $\begin{bmatrix} x_T & y_T \end{bmatrix}^T$ find θ_1)
 - a) $\cos(a^2 + a_2^2 a_1^2)$ b) $a_2^2 + a^2 2a_2 a \cos \theta_1$ c) $2a_2 a \cos \theta_1$ d) $\arccos \left| \frac{a^2 + a_2^2 a_1^2}{2a_2 a} \right|$

Solution

- This mechanism has **one** degree of freedom as it has only one *independent* joint variable (θ_1) and all other joints depend on it.
- Gruebler formula **can not** be used because the mechanism moves in one dimension (in the *x*-axis direction) only While Gruebler formula is used with either 2D or 3D.
- Manipulator Forward Kinematics
 - Since the mechanism is restricted to move in the *x*-axis direction only, then:

$$y_T = y_S = 0$$

- in figure, let *a* be the length of the triangle side formed by the three joints. We get:

$$x_T = d = a + a_3$$

- applying sine rule to the triangle:

$$\frac{\sin \theta_1}{a_1} = \frac{\sin \theta_2}{a_2} = \frac{\sin(\pi - \theta_3)}{a} \qquad = \frac{\sin[\pi - (\theta_1 + \theta_2)]}{a} = \frac{\sin(\theta_1 + \theta_2)}{a}$$
$$\theta_2 = \arcsin\left[\frac{a_2}{a_1}\sin\theta_1\right] \quad \Rightarrow \quad a = \frac{a_2\sin(\theta_1 + \theta_2)}{\sin\theta_1}$$
$$x_T = d = a + a_3 = a_3 + \frac{a_2\sin(\theta_1 + \theta_2)}{\sin\theta_1}$$

• Manipulator Inverse Kinematics

- at any time:

$$x_T = d = a + a_3 \quad \Rightarrow \quad a = x_T - a_3$$

– using cosine rule:

$$a_1^2 = a_2^2 + a^2 - 2 a_2 a \cos \theta_1 \quad \Rightarrow \quad \theta_1 = \arccos \left[\frac{a^2 + a_2^2 - a_1^2}{2a_2 a} \right]$$

Question 5. [24 Marks]

The Stäubli robot is an anthropomorphic robot with a spherical wrist as shown with its dimensions:

 (3×8)



21. According to the DH conventions, we can assign frames to the first three joints as:



22. The DH parameters of the **spherical** wrist joints:

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a)	Link	a_i	α_i	d_i	$ heta_i$		Link	a_i	α_i	d_i	$ heta_i$;
	4	0	-90	0	θ_4	b)	4	0	90	d_4	θ_4	Ł
а)	5	0	90	0	θ_5	6)	5	0	90	0	θ_5	j
	6	0	0	d_6	θ_6		6	0	0	d_6	θ_{ϵ}	;
c)	Link	a_i	α_i	d_i	θ_i		Link	a_i	0	x_i (d_i	ł
	4	0	0	d_4	θ_4	d)	4	0	9	0 0	d_4	6
	5	0	0	0	θ_5	u)	5	0	-9	0	0	6
	6	d_2	90	d_6	θ_6		6	0		0 0	d_6	θ

23. the homogeneous transformation matrices ${\cal A}_3$ is found as:

a)
$$\begin{bmatrix} c_3 & 0 & s_3 & 0 \\ s_3 & 0 & -c_3 & 0 \\ 0 & 1 & 0 & d_3 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$
b)
$$\begin{bmatrix} c_3 & -s_3 & 0 & d_3 c_3 \\ s_3 & c_3 & 0 & d_3 s_3 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$
c)
$$\begin{bmatrix} c_3 & 0 & s_3 & 0 \\ s_3 & 0 & -c_3 & 0 \\ 0 & -1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$
d)
$$\begin{bmatrix} s_3 & 0 & c_3 & 0 \\ c_3 & 0 & -s_3 & 0 \\ 0 & -1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

Solution

According to the DH conventions, we can assign frames to all joints as:



The DH parameters of the robot joints:

Link	a_i	α_i	d_i	$ heta_i$
1	0	90	d_1	θ_1
2	d_2	0	0	θ_2
3	0	-90	0	θ_3
4	0	90	d_4	θ_4
5	0	-90	0	θ_5
6	0	0	d_6	θ_6

The matrices describing the relative poses of the neighboring coordinate frames:

$$A_{1} = \begin{bmatrix} c_{1} & 0 & s_{1} & 0 \\ s_{1} & 0 & -c_{1} & 0 \\ 0 & 1 & 0 & d_{1} \\ 0 & 0 & 0 & 1 \end{bmatrix} A_{2} = \begin{bmatrix} c_{2} & -s2 & 0 & d_{2}c_{2} \\ s_{2} & c_{2} & 0 & d_{2}s_{2} \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} A_{3} = \begin{bmatrix} c_{3} & 0 & s_{3} & 0 \\ s_{3} & 0 & -c_{3} & 0 \\ 0 & -1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} A_{4} = \begin{bmatrix} c_{4} & 0 & s_{4} & 0 \\ s_{4} & 0 & -c_{4} & 0 \\ 0 & 1 & 0 & d_{4} \\ 0 & 0 & 0 & 1 \end{bmatrix} A_{5} = \begin{bmatrix} c_{5} & 0 & s_{5} & 0 \\ s_{5} & 0 & -c_{5} & 0 \\ 0 & -1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} A_{6} = \begin{bmatrix} c_{6} & -s_{6} & 0 & 0 \\ s_{6} & c_{6} & 0 & 0 \\ 0 & 0 & 1 & d_{6} \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

The geometric model of the robot arm is represented by the product of first three matrices:

$$H_3^0 = A_1 A_2 A_3 = \begin{bmatrix} c_1 c_{23} & -s_1 & -c_1 s_{23} & d_2 c_1 c_2 \\ s_1 c_{23} & c_1 & -s_1 s_{23} & d_2 s_1 c_2 \\ s_{23} & 0 & c_{23} & d_1 + d_2 s_2 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

Even more complex is the geometric model of robot wrist, represented by the product of the last three matrices:

$$H_6^3 = A_4 A_5 A_6 = \begin{bmatrix} c_4 c_5 c_6 - s_4 s_6 & -c_4 c_5 s_6 - s_4 c_6 & -c_4 s_5 & -d_6 c_4 s_5 \\ s_4 c_5 c_6 + c_4 s_6 & -s_4 c_5 s_6 + c_4 c_6 & -s_4 s_5 & -d_6 s_4 s_5 \\ s_5 c_6 & -s_5 s_6 & c_5 & d_4 + d_6 c_5 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

Supplementary Material

Note: you may need some or none of these identities:

$$R_{Z} = \begin{bmatrix} \cos\theta & -\sin\theta & 0\\ \sin\theta & \cos\theta & 0\\ 0 & 0 & 1 \end{bmatrix}, \quad R_{Y} = \begin{bmatrix} \cos\theta & 0 & \sin\theta\\ 0 & 1 & 0\\ -\sin\theta & 0 & \cos\theta \end{bmatrix}, \quad R_{X} = \begin{bmatrix} 1 & 0 & 0\\ 0 & \cos\theta & -\sin\theta\\ 0 & \cos\theta & -\sin\theta\\ 0 & \sin\theta & \cos\theta \end{bmatrix}$$
$$A_{i} = \begin{bmatrix} \cos\theta_{i} & -\cos\alpha_{i}\sin\theta_{i} & \sin\alpha_{i}\sin\theta_{i} & a_{i}\cos\theta_{i}\\ \sin\theta_{i} & \cos\alpha_{i}\cos\theta_{i} & -\sin\alpha_{i}\cos\theta_{i} & a_{i}\sin\theta_{i}\\ 0 & \sin\alpha_{i} & \cos\alpha_{i} & d_{i}\\ 0 & 0 & 0 & 1 \end{bmatrix}$$
$$\cos(a \pm b) = \cos(a)\cos(b) \mp \sin(a)\sin(b)$$
$$\sin(a \pm b) = \sin(a)\cos(b) \pm \cos(a)\sin(b)$$
$$\sin(\theta) = -\sin(-\theta) = -\cos(\theta + 90^{\circ}) = \cos(\theta - 90^{\circ})$$
$$\cos(\theta) = \cos(-\theta) = \sin(\theta + 90^{\circ}) = -\sin(\theta - 90^{\circ})$$
$$\cos^{2}(\theta) + \sin^{2}(\theta) = 1$$
$$\text{if } \cos(\theta) = b, \text{ then } \theta = \tan 2\left(\pm\sqrt{1-b^{2}}, b\right)$$
$$\text{if } \sin(\theta) = b, \text{ then } \theta = \tan 2\left(b, \pm\sqrt{1-b^{2}}\right)$$

For a triangle: $A^2 = B^2 + C^2 - 2BC\cos(a), \quad \frac{\sin(a)}{A} = \frac{\sin(b)}{B} = \frac{\sin(c)}{C}$

